

Topology optimization of heat conduction problems

Workshop on industrial design optimization for fluid flow
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Motivation and outline

➤ Challenges

- Topology optimization of coupled heat conduction and fluid flow
- Large scale systems: OpenFOAM
- FVM + Topology optimization + diffusion problems

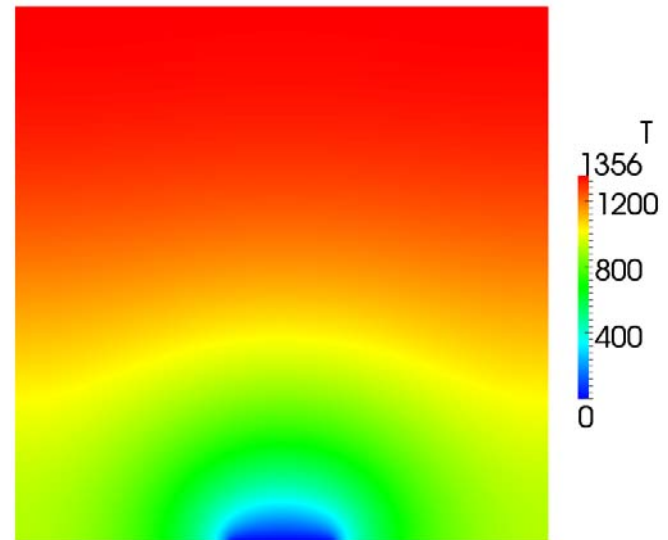
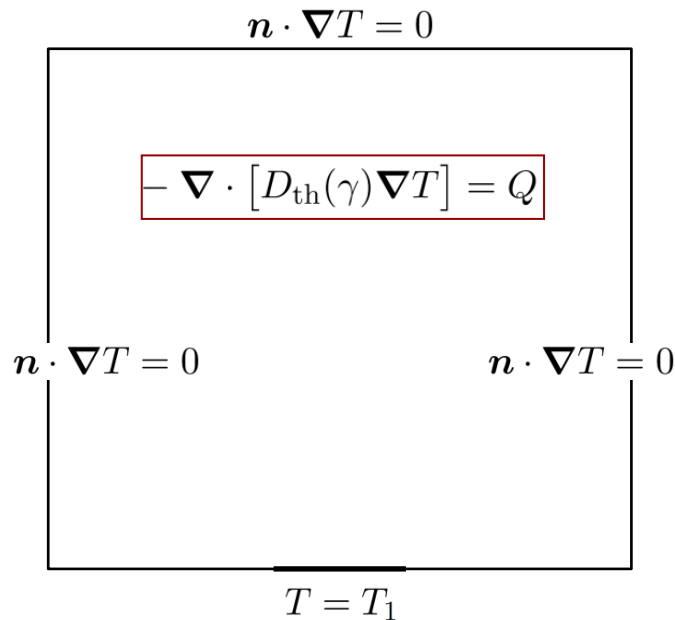
➤ Outline

- Optimization of simple conduction problem
- FVM on diffusion problems
- Constant convection added
- Preliminary tests of unstructured mesh and 3D

Simple heat conduction problem

➤ Pure heat conduction problem

- Constant and homogeneous heat source Q
- Insulating walls and heat sink at bottom $T_1 = 0$
- For topology optimization: Design dependent thermal diffusivity $D_{\text{th}}(\gamma)$



Topology optimization of conduction problem

➤ Topology optimization

- Minimize the weighted average temperature
- Distribution of two materials with different conductivity
- High conductivity D_{th2} : black (Max. volume 40%)
- Low conductivity D_{th1} : White
- $D_{th}(\gamma) = D_{th1} + (D_{th2} - D_{th1}) \gamma^3$, $D_{th2}/D_{th1} = 1000$

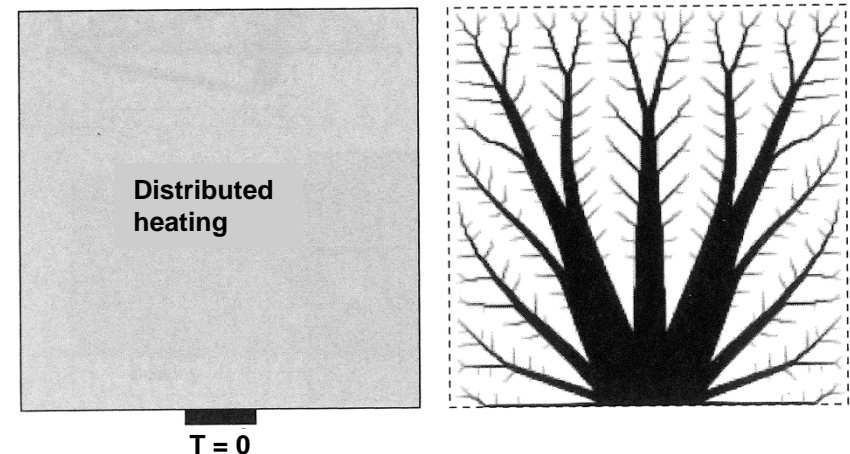
➤ IPOPT for the optimization routine

- Gradient based optimization
- Approximations of the hessian

➤ Benchmark example

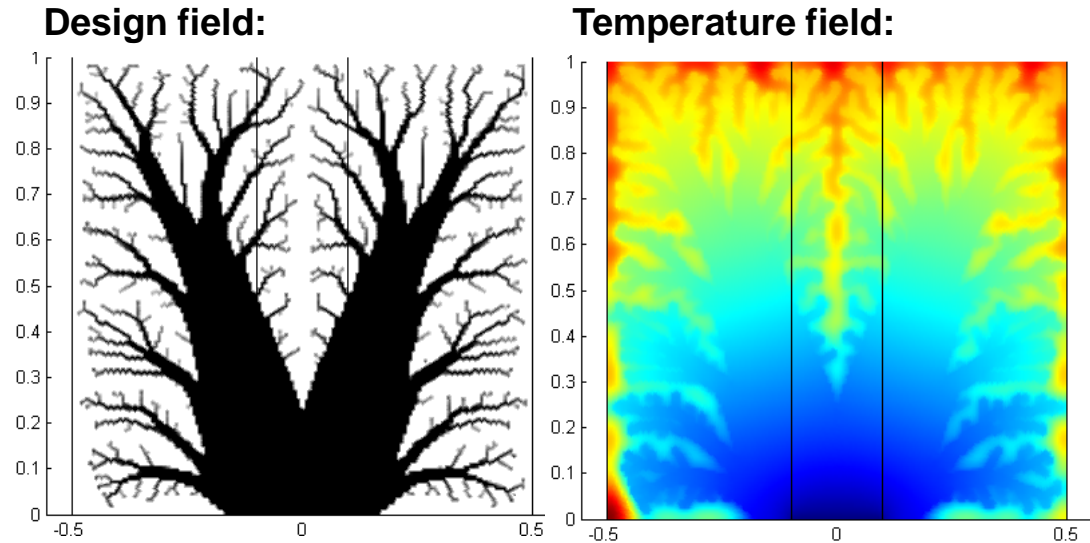
- FEM calculation
- MMA for the optimization loop

Bendsøe - Sigmund, Springer (2004)

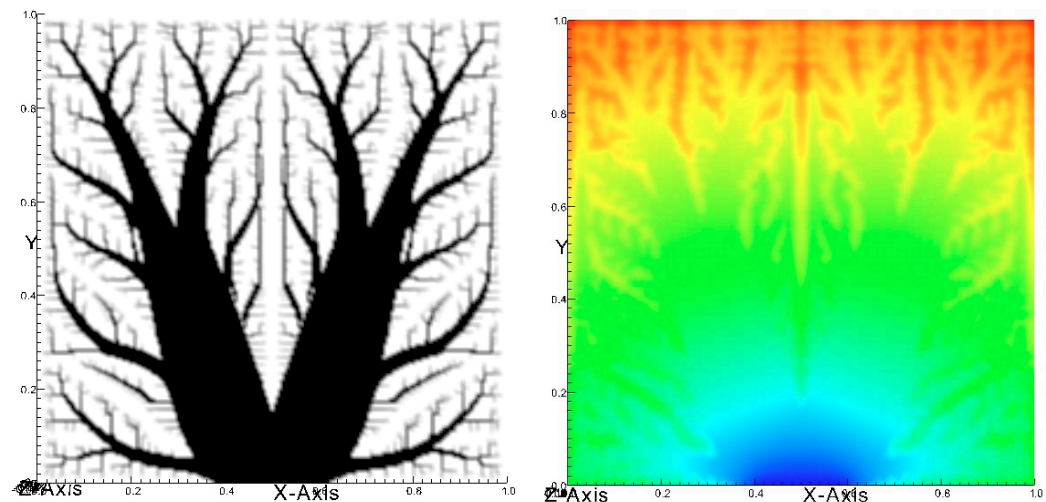


FVM \gg FEM optimization results

- **COMSOL (FEM)**
+ MMA
 - Unstructured mesh



- **OpenFOAM (FVM)**
+ IPOPT
 - Slightly different parameter values
 - Square mesh elements



New: FVM & TopOpt & conduction

➤ General form of balance law (steady state)

$$\nabla \cdot (F(u, \nabla u)) + s(u) = 0$$

➤ Previously studied: FVM & TopOpt for flow problems

- Design field enters the source term s

$$\rho(\mathbf{u} \cdot \nabla) \mathbf{u} = -\nabla p + \eta \nabla^2 \mathbf{u} - \underline{\alpha(\gamma) \mathbf{u}}$$

$$\nabla \cdot \mathbf{u} = 0$$

- For instance: **Othmer, Int. Jour. Num. Meth. Fluids (2008).**

➤ FVM & TopOpt for conduction problems

- Design field enters the flux term F

$$-\nabla \cdot [\underline{D_{th}(\gamma)} \nabla T] = Q$$

➤ Discretization using the FVM

- The flux term is integrated by parts:

Sensitivities becomes dependent on the design field gradient,

Sensitivity analysis of conduction problem

➤ Adjoint method

- Define a cost function

$$J = \int_{\Gamma} d\Gamma J_{\Gamma} + \int_{\Omega} d\Omega J_{\Omega}$$

- Define Lagrange function by introducing Lagrange multiplier λ

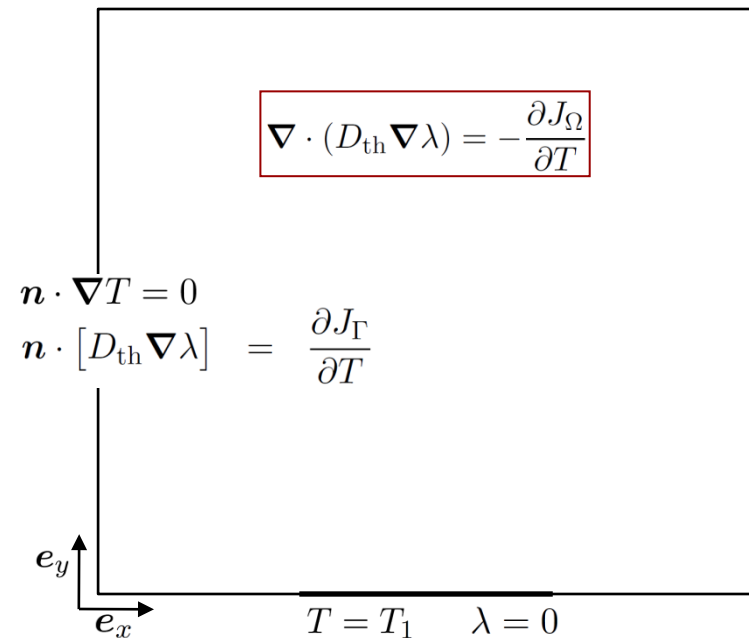
$$\mathcal{L} = J + \int_{\Omega} d\Omega \lambda R$$

- Solve the adjoint problem for λ (adjoint temperature)



- Calculate sensitivity

$$\frac{d\mathcal{L}}{d\gamma_i} = \int_{\Omega} d\Omega \lambda \nabla \cdot \left[\frac{\partial D_{\text{th}}(\gamma)}{\partial \gamma_i} \nabla T \right]$$



Continuous vs. discrete adjoint

➤ FVM

- Gradient approximation on cell edges
- Imprecise for discontinuous fields

➤ Continuous adjoint

- Optimize (differentiate) then discretize
- Sensitivity:
$$\frac{d\mathcal{L}}{d\gamma_i} = - \int_{\Omega} d\Omega \frac{\partial D_{th}(\gamma)}{\partial \gamma_i} \nabla \lambda \cdot \nabla T$$

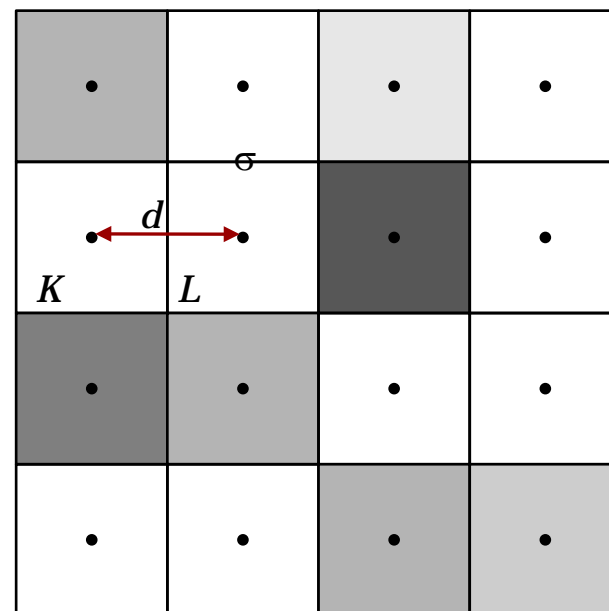
➤ Sensitivity for flow problem

- Adjoint and primary flow velocity; u, v
- Sensitivity:
$$\frac{d\mathcal{L}}{d\gamma_i} = \int_{\Omega} d\Omega \frac{\partial \alpha(\gamma)}{\partial \gamma_i} u \cdot v$$

➤ Discrete adjoint

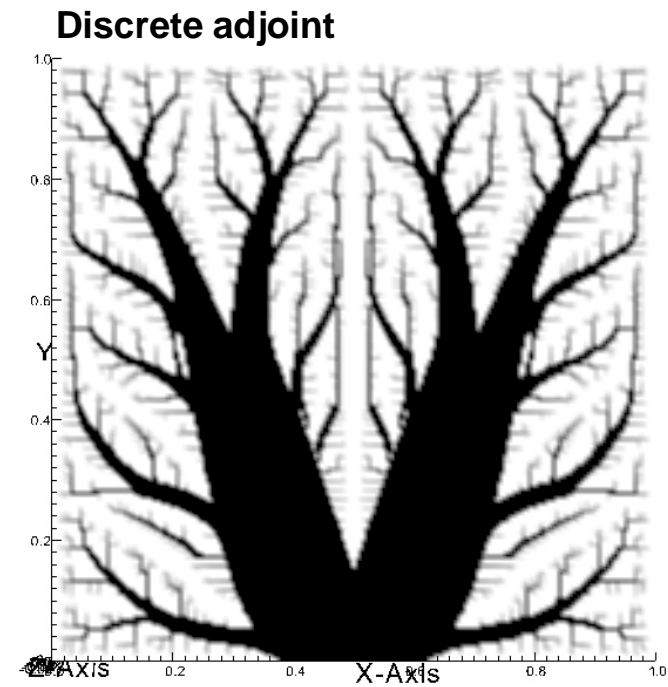
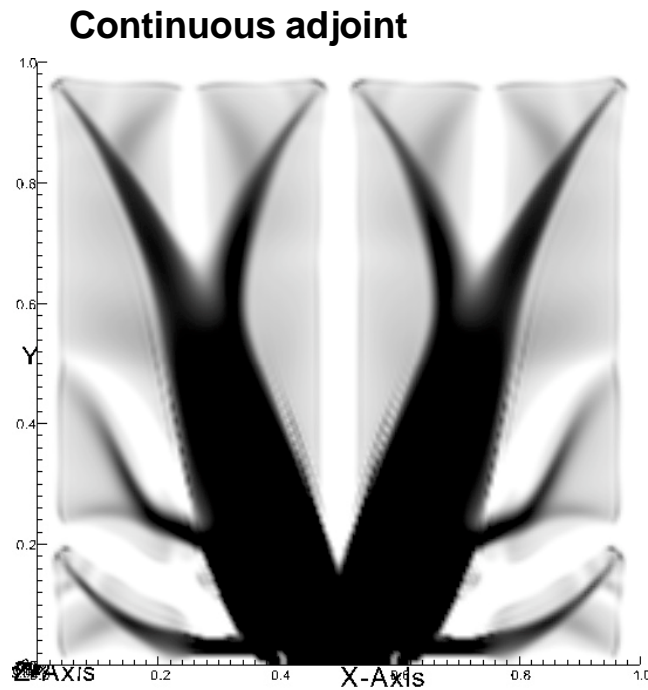
- Discretize then optimize (differentiate)
- Sensitivity:
$$\frac{d\mathcal{L}}{d\gamma_i} = \sum_{\sigma_i} \frac{|\sigma_i|}{d_{KL}} \frac{\partial D_{th}}{\partial \gamma_i} (T_K - T_L) (\lambda_K - \lambda_L)$$

Discretized design field γ



Discrete \gg continuous optimizations

- Different optimization output depending on parameters



Further numerical considerations

➤ Mesh convergence

- **Proof lacking: Discretized continuous adjoint sensitivity should converge to continuous expression**
- **Expect unaltered topology, but feature refinement can cause problems**
 - Continuous adjoint: Volume integration -> small sensitivity change
 - Discrete adjoint: Cell edge integration -> large sensitivity change

➤ IPOPT

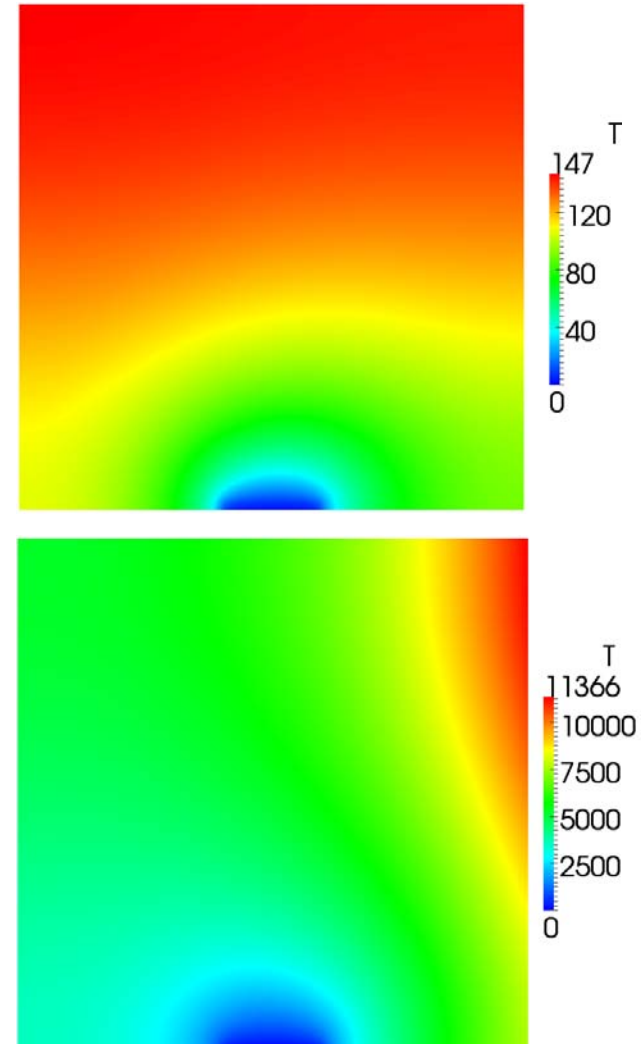
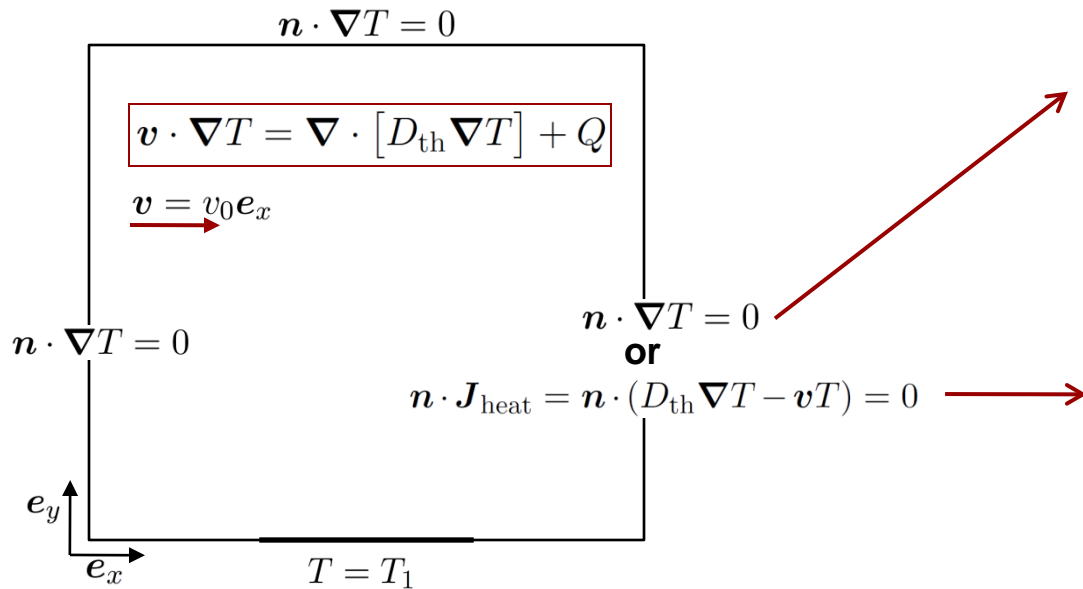
- **Robust optimization routine**
- **Poor hessian approximations on top of uncertain gradient approximations**
- **MMA might be more suitable (no hessian needed)**

➤ Higher order approximations of fluxes

- **Unsuitable for fields with large discontinuities across cell boundaries**

Conduction – convection model

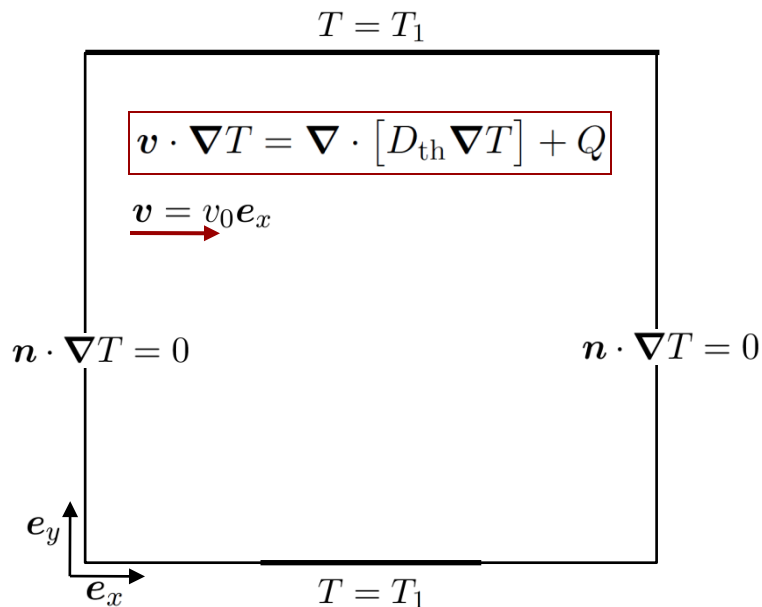
- Constant convection term added
- Insulation BC: Robin condition
 - Non-trivial implementation in OpenFOAM



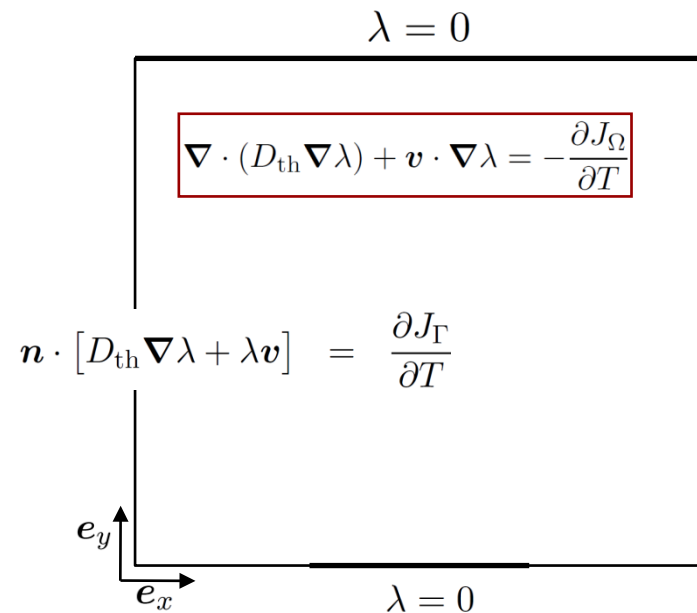
Adjoint equations for convection-conduction problem

- Robin BC in the adjoint problem
- Heat sink added at upper boundary

Primary problem:

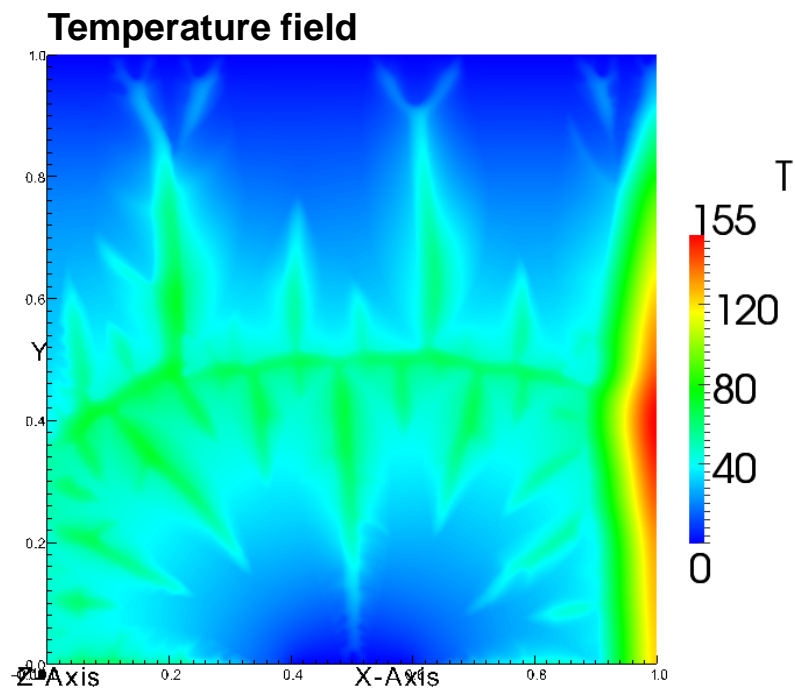
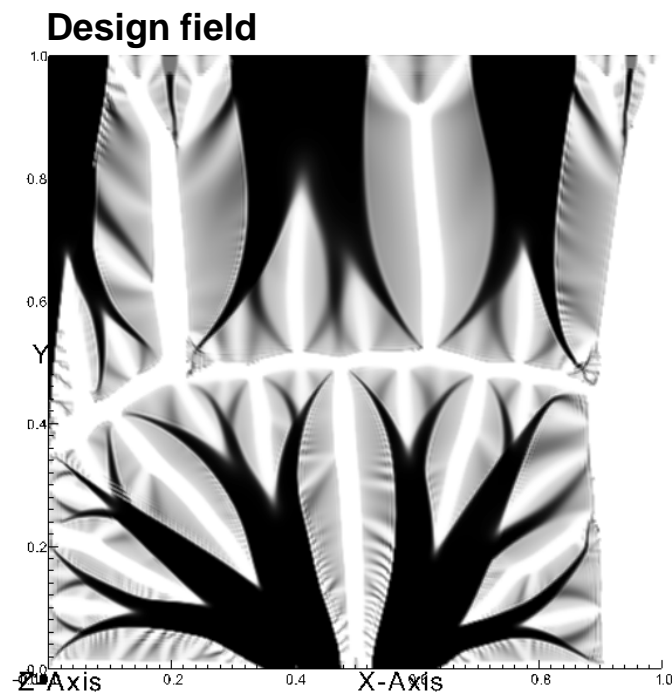


Adjoint problem:



Preliminary conduction-convection optimization

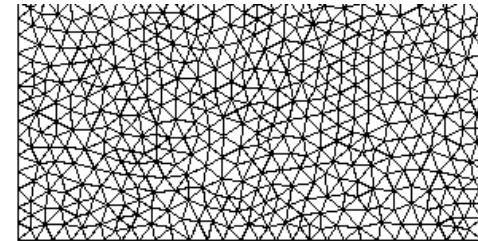
- Minimize the weighted average temperature
- Continuous adjoint



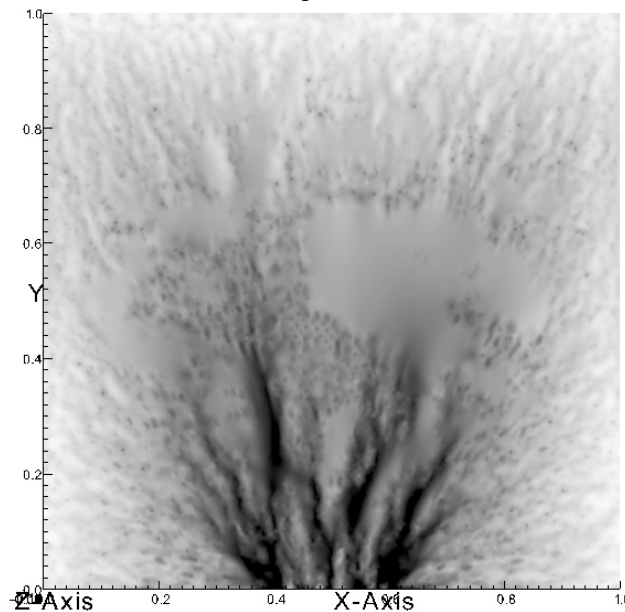
Unstructured mesh – preliminary results

- Pure conduction problem
- Influence of adjoint method

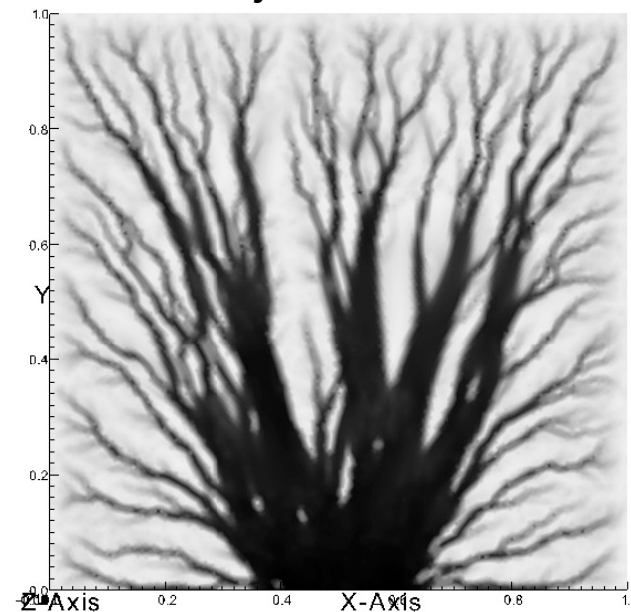
Section of mesh



Continuous adjoint



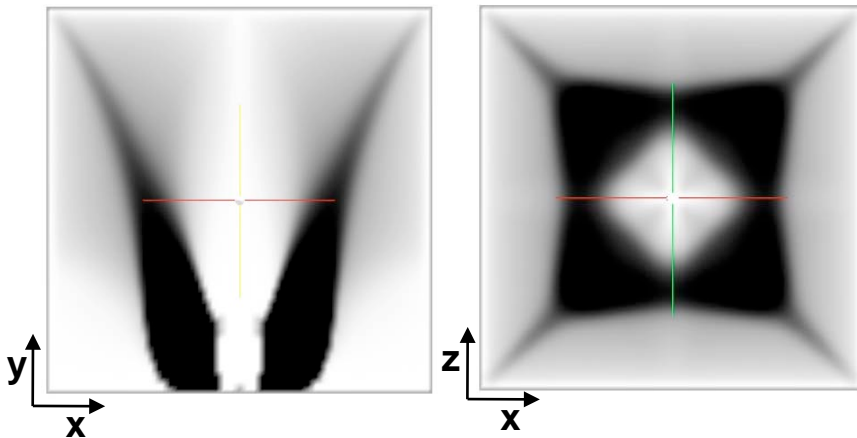
Discrete adjoint



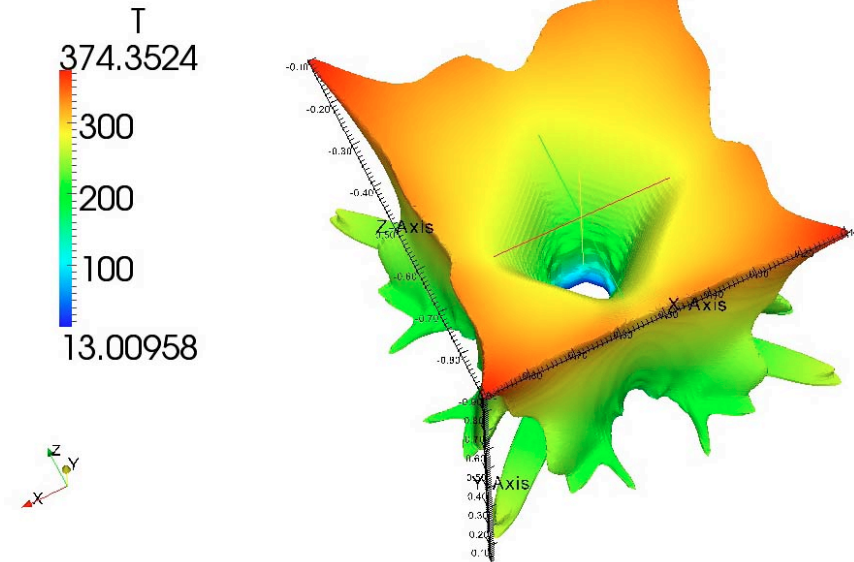
Preliminary 3D result

➤ Pure conduction problem

Cross-sectional plots of design field γ :



Contour surface at $\gamma = 0.8$
Color plot of temperature field



➤ Parallelization

- Decomposition of computational domain (OpenFOAM)
- Parallelization of optimization routine (MMA)

Summary and outlook

➤ Summary

- Topology optimization of heat conduction problem with IPOPT & OpenFOAM
- Comparison with COMSOL & MMA
- Identified numerical issues for FVM based topology optimization of diffusion problems
- Implemented discrete adjoint method for regular (and unstructured) meshes
- Implementation of optimization routine for constant convection problem
- Preliminary results of: conduction-convection problem, 3D heat conduction problem, unstructured mesh

➤ Outlook

- Parallelization of optimization routine (MMA)
- Coupling to the Navier-Stokes equation
- Optimization of fully coupled heat transfer problem for a simple model case

