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CAD-based shape optimisation using a discrete adjoint solver

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- > Parameterisation is the key to successful optimisation
 - Node-based optimisation interface not well with CAD
 - Full CAD-based approach needs either (1) differentiating the CAD system or (2) solving transformation matrix using finite difference





Figure: Node-based (left) v.s. full CAD-based (right)optimisation.

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Figure: Node-based (left) v.s. full CAD-based (right)optimisation.

A more flexible CAD-based optimisation is needed

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 Use the control points of the boundary representation (BRep) as design parameters



Figure: Surface with control points (C.P.) viewed in CAD.

Advantages: good interface to CAD, no smoothing/fd
 Challenge: imposition of various constraints

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Boundary representation, definition of NURBS

 Surfaces in CAD systems are NURBS (Non-Uniform Rational B-Spline), defined as follows

$$X_{s}(u, v) = \sum_{i=0}^{n} \sum_{j=0}^{m} R_{ij}(u, v) P_{i,j}$$
$$R_{ij}(u, v) = \frac{N_{i,p}(u)N_{j,q}(v)w_{i,j}}{\sum_{k=0}^{n} \sum_{l=0}^{m} N_{k,p}(u)N_{l,q}(v)w_{k,l}}$$

 Position, tangent vectors and curvatures can be computed inexpensively for imposing (nonlinear) continuity constraints

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Test points for imposing constraints

 Continuity is enforced at test points located along the joint edge



Figure: Schematic of test points distributed along the joint edge.

Constraint functions evaluated at test points

$$C_{G0} = (X_s)_{left} - (X_s)_{right} = 0$$

$$C_{G1} = (\vec{\tau})_{left} \times (\vec{\tau})_{right} = 0$$

$$C_{G2} = (k)_{left} - (k)_{right} = 0$$

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Imposing continuity constraints using nullspace

 Control points are only allowed to move within the nullspace of the linearized constraint equations

$$\frac{\partial C_{Gi}}{\partial P_i} dP_i = 0 \ (i = 0, 1, 2)$$
$$\implies \delta \vec{P} = \operatorname{Ker} \left(\frac{\partial C_{G0}}{\partial P}, \frac{\partial C_{G1}}{\partial P}, \frac{\partial C_{G2}}{\partial P} \right) \delta \vec{\alpha}$$

Nonlinear constrains G1 and G2 can be dealt with

 Nullspace is independent of mesh size, thus remains inexpensive to compute for large cases CAD-based Opt

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S-bend shape optimisation, case parameters

- Geometry parameterisation: 30 NURBS patches, with 8 patches for "S" with 288 C.P.
- ▶ 203 design variables, 313,925-cell mesh, *Re_H*=300
- Solver: in-house incompressible discrete adjoint solver



Figure: NURBS patches (left) and all-hex mesh (right).

(Ref: D. Jones, J.-D. Müller and S. Bayyuk, CFD Development with Automatic Differentiation, AIAA-2012-573)

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S-bend shape optimisation, primal validation

- Small separation bubble about to reach pressure outlet
- Flow speed contour plots at outlet indicate complex secondary flow



Figure: Flow speed contour plots in medien plane and outlet boundary plane, GPDE v.s. FLUENT.

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Literation 1 ΔP = 0.015182 Pa Improvement 0.60%

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Literation 2 ΔP = 0.014839 Pa Improvement 2.84%

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Unexpected shape at 6th iteration



Figure: Updated shape at 6th iteration.

Possible cause for failure

 Interference from non-vanishing large sensitivity at S-bend throat ⇒ allow the throat to deform

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Summary

A novel CAD-based optimisation method is developed, using the control points of the boundary representation (BRep) for parameterisation

- Good interface with CAD
- Continuity constraints easy to impose
- Extendable to more complex geometry
- Cost is negligible compared to flow solver

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Future work

- Short-term (Apr. 2012)
 - Implementation of G2 constraint
 - Extend to more complex geometries



Figure: Examples of more complex geometric entities.

- Long-term (May 2011- May 2013)
 - Apply to turbomachinery components, such as compressor/turbine blade shape optimisation

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Thank you! Questions?